

H24 火山性流体討論会 & 地殻流体シーズナルスクール

岩石組織形成に対する粒間流体の役割

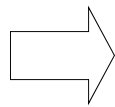
地球深部流体の物理化学的性質： 基礎をはじめに復習

“Geological fluids (地質流体)” の種類(主成分)

- 水(液体・気体)
- 超臨界水・超臨界CHO系流体
- 珪酸塩メルト
- 珪酸塩メルトと超臨界水の混和状態
- 炭酸塩メルト(カーボナタイト)
- 硫化物メルト
- (溶融金属)

“Geological fluids” (地質流体)の役割

- 固体に比べて圧倒的に速く物質と熱を運搬する
- 固体と物性が大きく異なる
(流体を含む岩石は物性が大きく変わる)



地球の化学進化
地球のダイナミクス

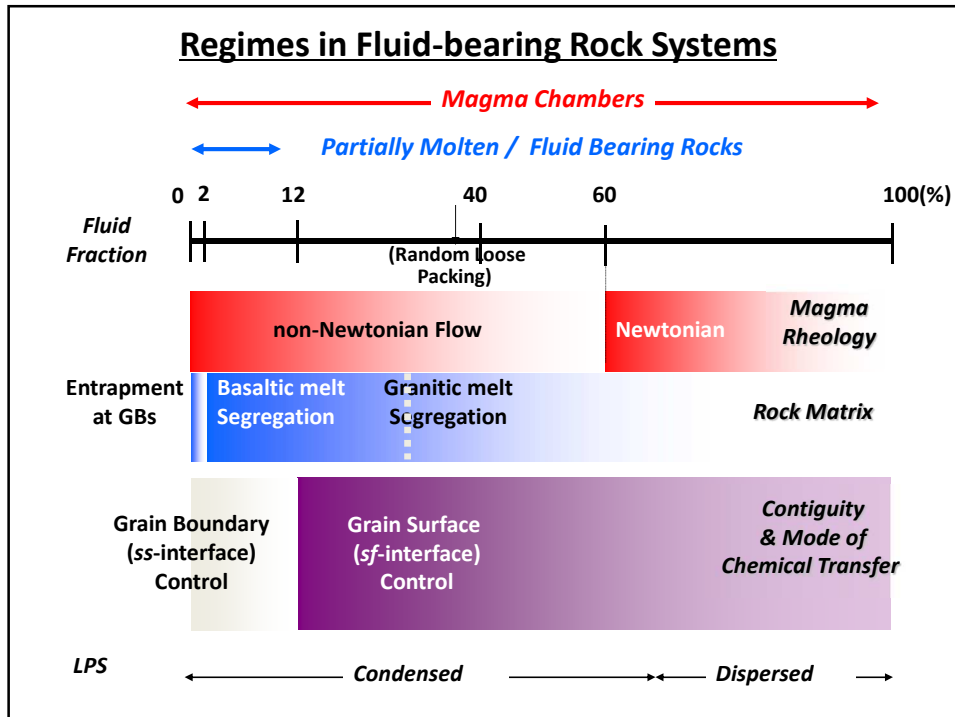
流体の関与する重要な現象の例

- ☆ 変成作用・岩石-水反応
- ☆ 鉱床形成・鉱化作用
- ☆ フラックス融解
- ☆ 部分溶融マントル・地殻からのメルトの分離
- ☆ マグマ溜まりプロセス
- ☆ マントルメタソマティズム
- ☆ 核形成

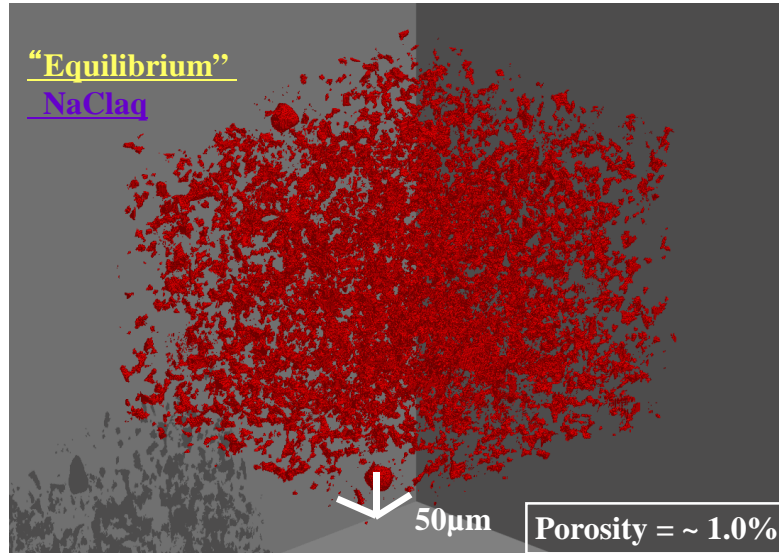
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流体の存在量・岩石微細構造に
強く依存する岩石物性

- + 密度 Density
- + 粘性 Viscosity
- + 浸透率 Permeability
- + 全岩での拡散係数 Bulk diffusivity
- + 弾性波速度(異方性)
- + 電気伝導度
-



1%の流体とはどれくらいの量？



水の三態と臨界点

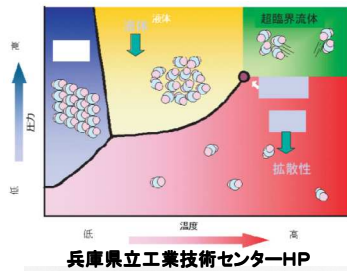


Figure 17.6 Phase diagram for H₂O at relatively low pressures. The solid-liquid boundary is very steep, but in fact has a negative slope.

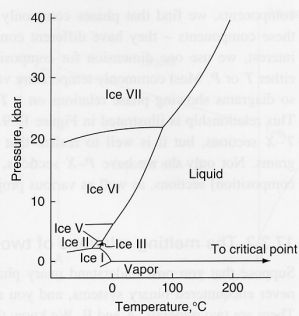
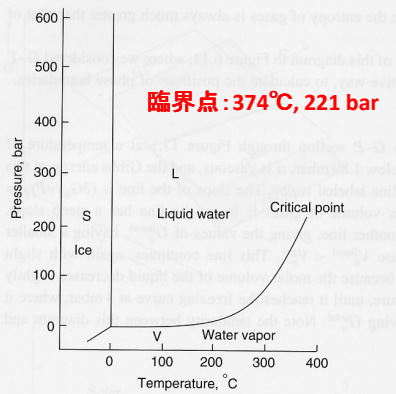
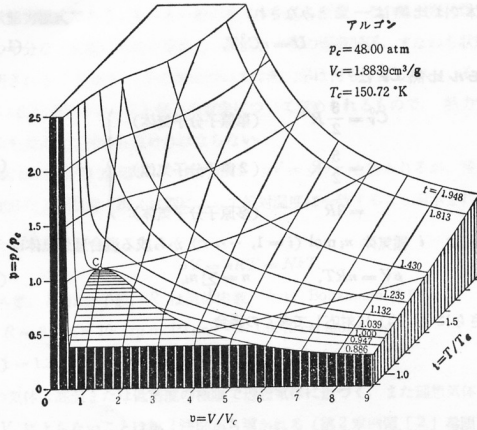


Figure 17.7 Phase diagram for H₂O at high pressures. Ice IV, not shown, is a metastable form of ice in the region of Ice V.

超臨界流体は、液体の高い分子密度と気体の大きい分子運動エネルギーを兼ね備える

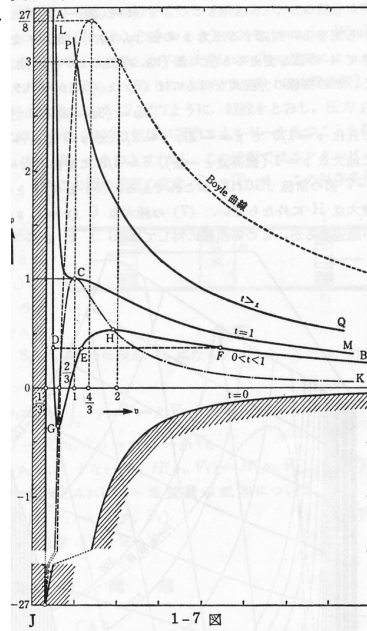
臨界点と超臨界流体



1-4 図 アルゴンの状態方程式のレリーフ

実在気体の状態方程式の例 (van der Waals の式)

$$\left(P + \frac{a}{V^2}\right)(V - b) = RT$$



1-7 図

久保亮吾 熱学統計力学 裳華房

圧縮因子と臨界定数

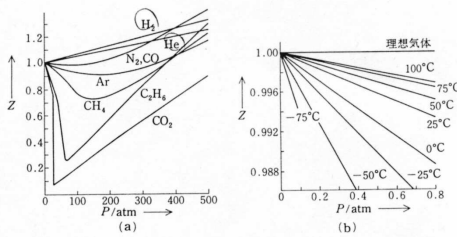


図 1-3 (a) 圧縮率因子の圧力変化 (温度はエタン (37°C) 以外は 0°C)
 (b) アルゴンの圧縮率因子の温度依存性

表 1-3 単体および無機化合物の臨界定数 (1 atm = 101325 Pa)

化学式	t_c °C	P_c atm	$\frac{V_c}{V_c^*}$ $\frac{p_c}{g \cdot cm^{-3}}$	$\frac{P_c V_c}{RT_c} \left(= \frac{P_c M}{RT_c \rho_c} \right)$
Ar	-122.4	48.1	0.533	0.291
Br ₂	311	102	1.36	0.288
CO	-140.24	34.53	0.301	0.294
CO ₂	31.0	72.8	0.468	0.274
CS ₂	279	78	0.44	0.298
D ₂	144	78	0.573	0.275
Cl ₂	-234.9	16.3	0.0660	0.313
F ₂	-128.85	51.47	0.574	0.288
HBr	90.0	84.4	—	—
HCl	51.5	82.0	0.45	0.249
HI	159.8	82	—	—
H ₂	-240.17	12.76	0.0314	0.303
H ₂ O	373.99	217.6	0.32	0.230
H ₂ S	100.0	88.2	0.346	0.283
He	-267.96	2.24	0.0698	0.303
NH ₃	132.4	111.3	0.235	0.242
NO	-93	64	0.52	0.250
NO ₂	158	100	0.55	—
N ₂	-147.0	33.5	0.313	0.292
Ne	-228.75	27.2	0.484	0.312
O ₂	-118.57	49.77	0.436	0.288
O ₃	-12.1	55	0.54	0.228
PH ₃	51.6	64.5	—	—
SF ₆	45.54	37.10	0.736	0.282
SO ₂	157.6	77.81	0.525	0.306
Xe	16.583	57.64	1.11	0.290

物理化学の基礎 西川・渡辺 学術図書 1979

超臨界流体の熱力学的性質

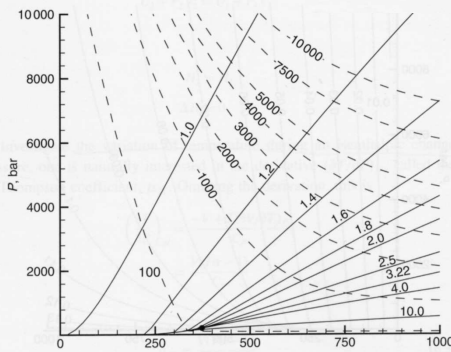
Specific volume

$$\left(\frac{\partial G}{\partial P}\right)_T = V$$

$$\int_{P_1}^{P_2} dG = \int_{P_1}^{P_2} V dP$$

$V=V(P, T)$: 状態方程式

Figure 6.1 The specific volume ($\text{cm}^3 \text{g}^{-1}$) of water as a function of P and T . Dashed contours are water fugacity in bars. Small dot indicates the critical point. Data from the program STEAM (§13.6.1)



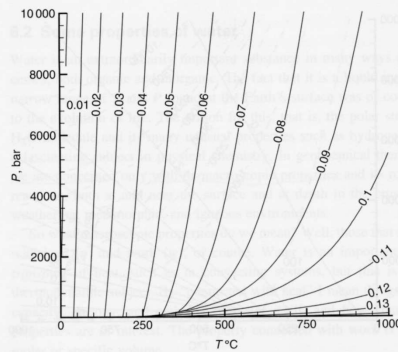
臨界点: 374°C, 221 bar,
3.22 $\text{cm}^3 \text{g}^{-1}$

Entropy

$$\left(\frac{\partial P}{\partial T}\right)_S = \frac{T}{C_p} \left(\frac{\partial V}{\partial T}\right)_P$$

> 0

Figure 6.2 The entropy of water in kJ mol^{-1} as a function of P and T . Data from the program STEAM of Harvey et al. (2000).



Anderson GM, Thermodynamics of Natural System, 2nd ed., Cambridge, 2005

C.E. Manning / Earth and Planetary Science Letters 223 (2004) 1–16

Critical end points

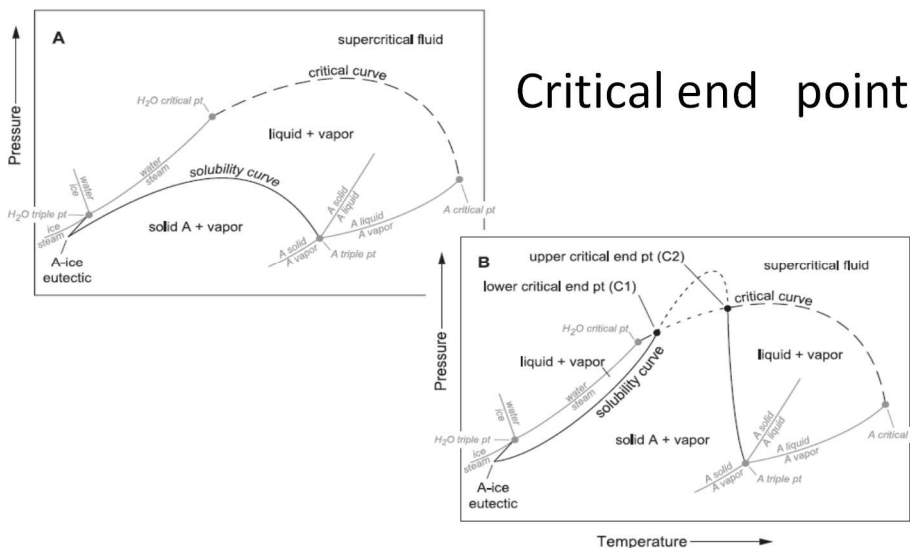
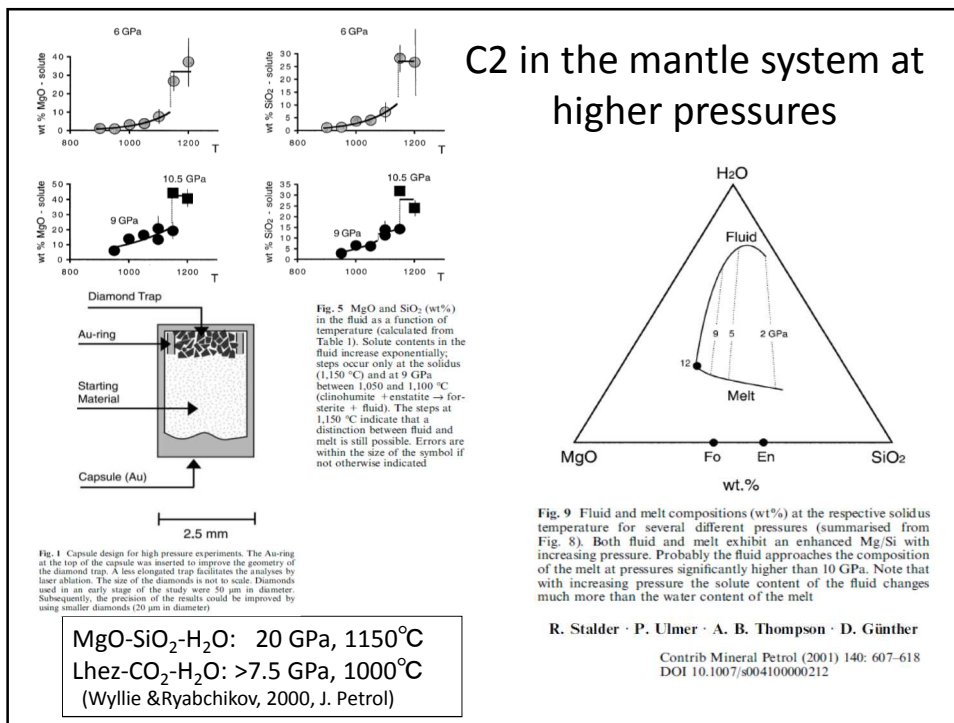
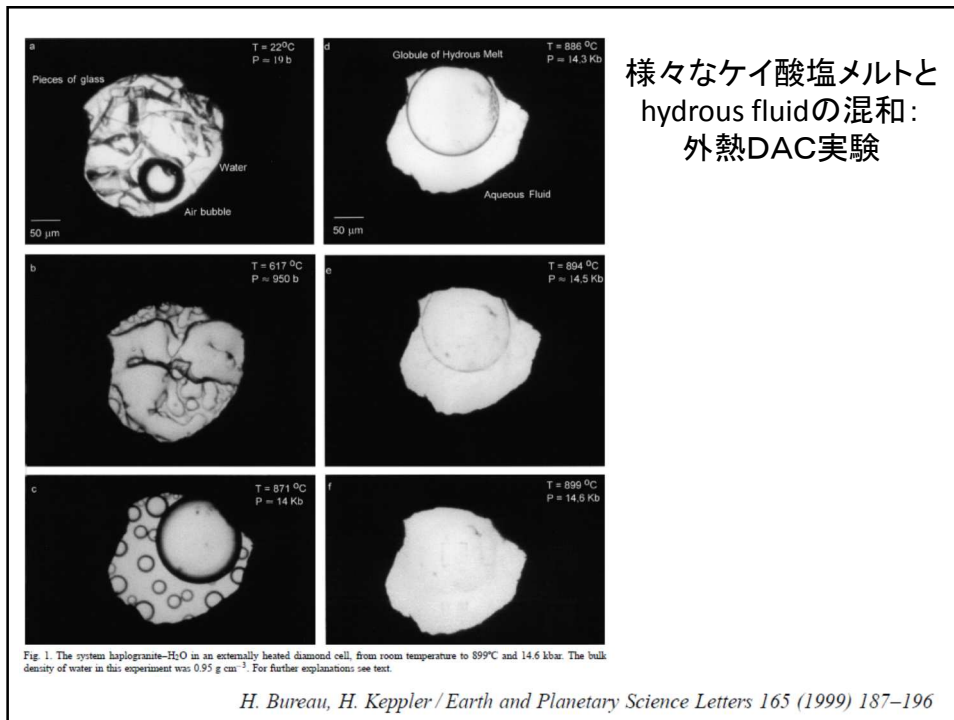
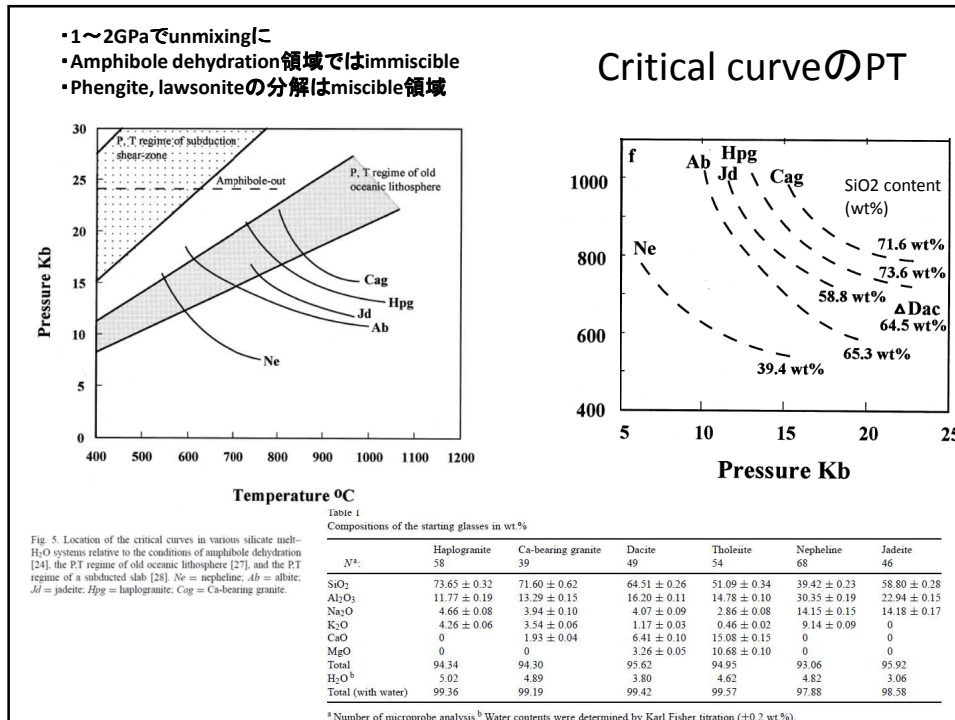
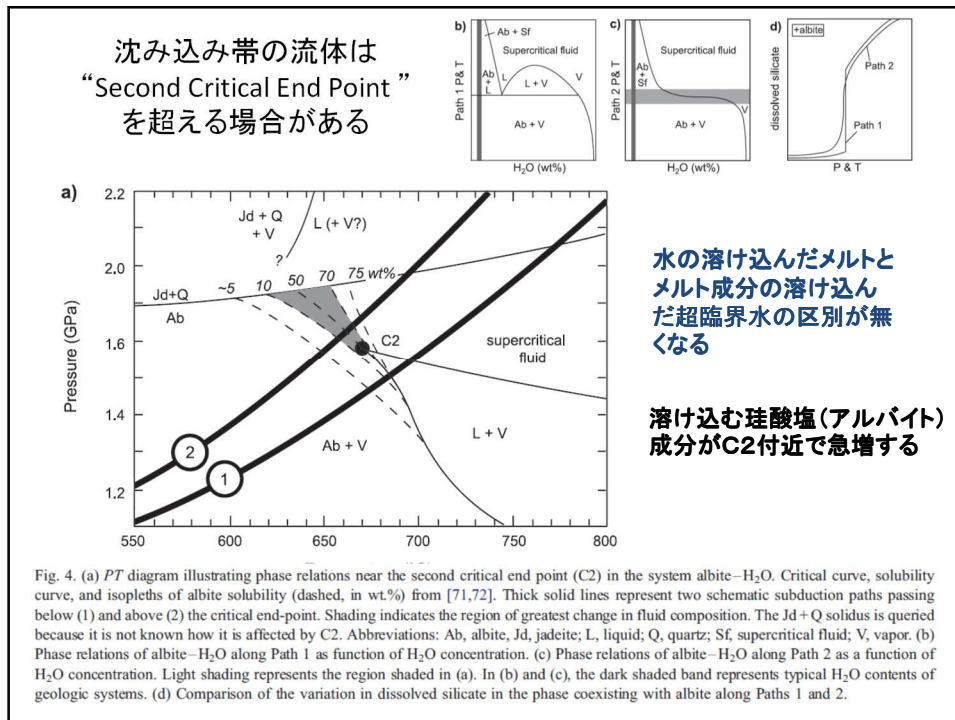


Fig. 3. Schematic P - T projections of phase relations illustrating contrasting behavior of simple two-component systems. Grey lines indicate phase relations for one-component systems H_2O and hypothetical composition A ; black lines represent relations for A - H_2O mixtures. Labeling of fields is for H_2O -rich systems. (A) The system A - H_2O , in which the critical curve and solubility curve do not intersect. NaCl - H_2O is an example of such a system. (B) The system A - H_2O , in which the critical curve and solubility curve intersect. This yields two critical end points (C1 and C2). Short dashed lines denote metastable portions of curves. Albite- H_2O is an example.





haplogranite-H₂O系 solvus (12.5 ~ 16.9 kb)

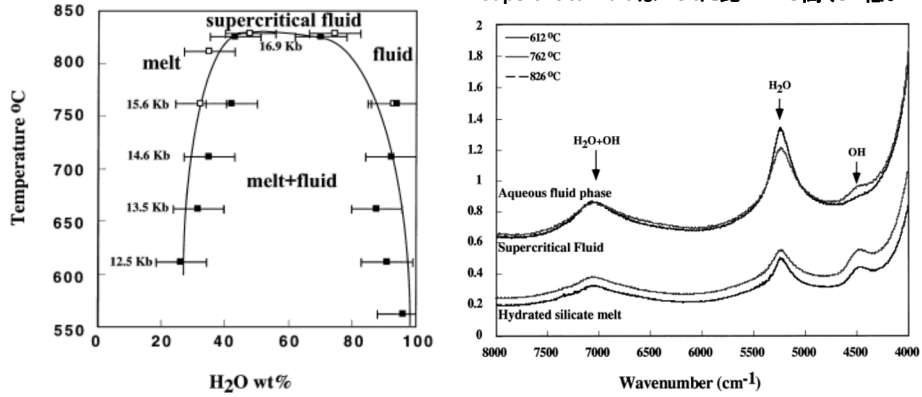
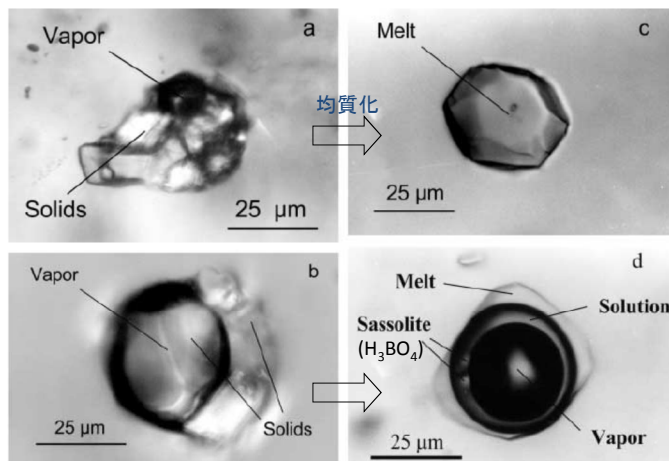


Fig. 4. Phase diagram of the system haplogranite-H₂O under isochoric conditions for a bulk density of water of 1.016 g cm⁻³. The compositions of the coexisting phases were derived from in-situ FTIR spectra. Open and closed symbols refer to two different sets of measurements.

- Hydrous fluid中のsilicate成分濃度は低い
- solvus頂部がflat

F, B, P の効果: ごく低圧(1kb)で珪酸塩メルトと熱水が完全混和



pegmatite中のmelt inclusion

R. Thomas · J. D. Webster · W. Heinrich
Contrib Mineral Petrol (2000) 139: 394-401

Fig. 1 Melt inclusions in pegmatite quartz from Ehrenfriedersdorf, Germany. a A-type melt inclusion. Solids (feldspars, quartz, mica, and others) occupy about 80% of the total inclusion volume. b B-type melt inclusion. Solids (feldspars, quartz, mica, and others) occupy about 60% of the total inclusion volume. c A-type melt inclusion, completely rehomogenized at 650 °C and 1 kbar. d B-type melt inclusion, completely rehomogenized at 650 °C and 1 kbar. Phase separation into glass, liquid, and vapor occurred during quenching

1 kbでのsolvus (均質化実験結果)

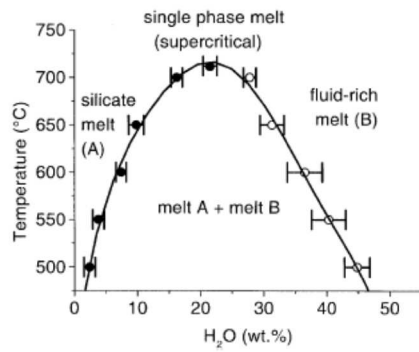


Fig. 3 Pseudobinary wt% H₂O versus temperature plot of rehomogenized A-type (closed circles) and B-type melt inclusions (open circles) in pegmatite quartz Qu8 from Ehrenfriedersdorf, Erzgebirge, Germany. Pressure is ~1 kbar

- ほぼimmiscible “melts”
- solvus頂部が狭い

Table 2 Representative oxide and element concentrations in the A-type and B-type melt inclusions homogenized at 650 °C and 1 bar. *d.l.* Detection limit, *n.d.* not determined

	A-type inclusion	B-type inclusion (glass portion)	B-type inclusion (glass + solution ^a)
SiO ₂	64.50 ± 1.09	61.08 ± 1.2	37.98 ^b
TiO ₂	0.02 ± 0.01	d.l.	–
SnO ₂	0.10 ± 0.02	0.80 ± 0.06	0.48 ^b
Al ₂ O ₃	11.69 ± 0.52	14.04 ± 0.77	8.74 ^b
B ₂ O ₃	0.20 ^c	n.d.	4.12 ^d
FeO	0.29 ± 0.05	2.04	1.27 ^b
MnO	0.04 ± 0.01	0.15	0.07 ^b
MgO	d.l.	d.l.	–
CaO	0.03 ± 0.01	d.l.	–
Na ₂ O	3.20 ± 0.14	3.33 ± 0.56	2.85
K ₂ O	3.01 ± 0.55	3.33 ± 0.43	3.37
Rb ₂ O	0.44 ± 0.04	0.55	> 0.35 ^b
Cs ₂ O	0.12	1.49 ± 0.24	0.92 ^b
P ₂ O ₅	3.20 ± 0.31	0.92	0.57 ^b
F	4.50 ± 0.25	4.19	2.60 ^b
Cl	0.14 ± 0.02	0.35 ± 0.02	5.78
H ₂ O	9.80 ± 1.2	9.0 ± 0.7	31.80 ^e
Sum	101.28	101.27	100.90
ASI	1.32	1.42	0.99

^aThe aqueous phase contains 8.5 ± 1.1 wt% NaCl eq.; NaCl/KCl ~1 (from cryometric measurements)

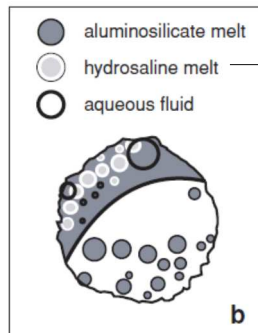
^bCalculated assuming presence only in the glass portion

^cDetermined by ion microprobe (SIMS) at Woods Hole Oceanographic Institution, MA, USA, as a maximum (see Webster et al. 1997)

^dCalculated from the boron acid (H₃BO₃) concentration in the liquid of B-type melt inclusions. According to the melting temperature of 51 ± 1.5 °C of the sassolite daughter crystals, a concentration of 10.5 wt% H₃BO₃ in the liquid was estimated

^eValue from Table 1

三相不混和流体の例



A starting glass with the bulk composition (in wt%): SiO₂ = 58.7, Al₂O₃ = 16.5, B₂O₃ = 5.0, Na₂O = 2.9, K₂O = 3.7, Rb₂O = 1.1, Cs₂O = 1.0, Li₂O = 0.5, P₂O₅ = 4.2, F 4.6, and H₂O = 1.5 was

contains (in wt%): SiO₂ = 23.2, Al₂O₃ = 21.4, B₂O₃ = 15.6, Na₂O = 5.1, K₂O = 2.4, Rb₂O = 1.1, Cs₂O = 1.0, P₂O₅ = 2.6, F = 17.5, the remaining 18% being mostly H₂O and minor Li₂O.

(550°C, 0.2GPa)

FIGURE 1. Photomicrograph (a) and explanatory sketch (b) of a plan view into the sample chamber of HDAC during slow cooling from 830 to 810 °C and -0.4 GPa. Globules of hydrosaline melt and fluid bubbles nucleated and grew inside aluminosilicate melt while beads of the aluminosilicate melt precipitated from the hydrous fluid implying close approach to thermodynamic equilibrium. The diameter of the sample chamber is 0.4 mm.

Determination of liquid/vapor partitioning of Cu and Zn by using synthetic fluid inclusion method and SR-XRF

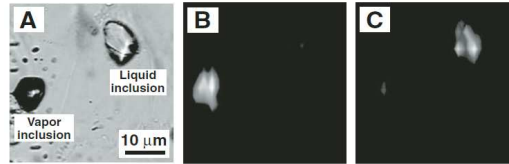


Figure 1. Typical example of Cu and Zn measurement in fluid inclusions synthesized under sulfur-rich conditions (run 18B). A: Optical microscopic image of X-ray irradiated area. Both vapor-rich and liquid-rich inclusions are present. B: Fluorescent X-ray image of Cu showing concentration in the vapor inclusion. C: Fluorescent X-ray image of Zn showing concentration in the liquid inclusion.

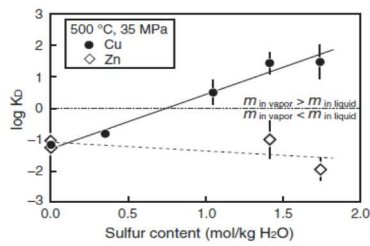


Figure 3. Vapor-liquid distribution constant ($\log K_D$) for Cu and Zn and its dependence on sulfur content at 500 °C and 35 MPa.

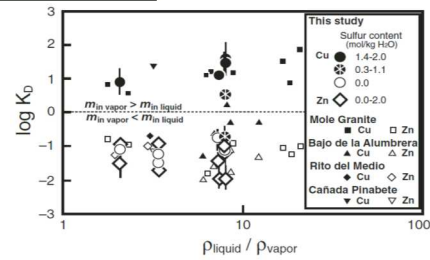


Figure 4. Comparison of $\log K_D$ values for Cu and Zn obtained in this study (both S-bearing and S-free experiments) with natural samples. Analytical data for coexisting vapor- and liquid-rich inclusions in hydrothermal ore deposits are from the Mole Granite (Audétat et al., 2000), the Bajo de la Alumbreira (Ulrich et al., 2001), the Rito del Medio pluton (Audétat and Pettko, 2003), and the Cañada Pinabete pluton (Audétat and Pettko, 2003).

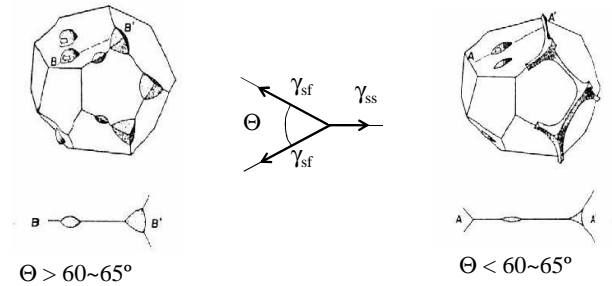
Nagaseki H. & Hayashi K.

Geology, January 2008; v. 36; no. 1; p. 27–30; doi: 10.1130/G24173A.1

岩石中での超臨界流体の分布形態と
移動様式

粒子スケールでの流体分布・連結度の
支配要因：“二面角”と流体量

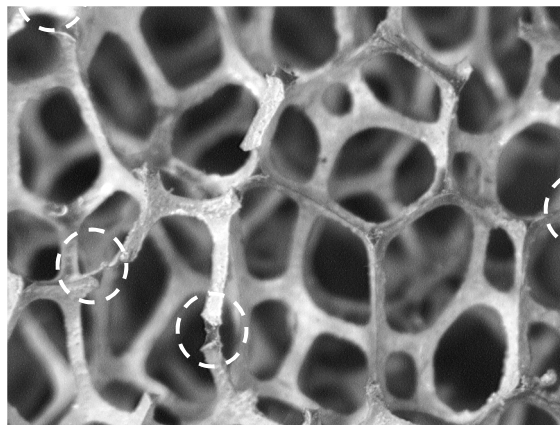
(理想的で単純な系)



流体は少量では連結せず孤立する
→浸透流として流れず、割れ目が必要

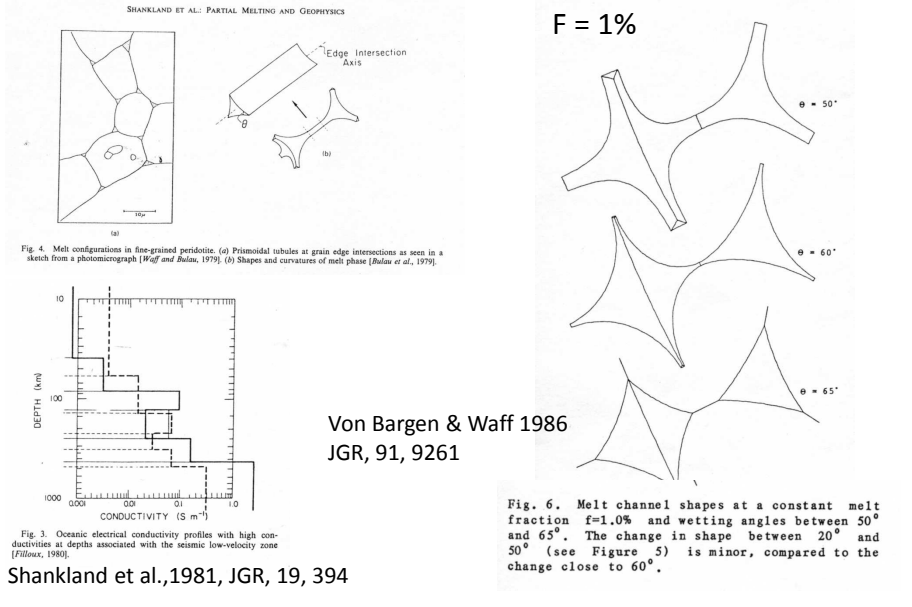
流体は少量で連結する
→浸透流になり得る

岩石中における連結した流体(二面角小)の形状
(イメージ)



流体の巨視的な移動様式は粒子サイズでの流体の形状に依存する。
←流体の形状は、結晶と流体の濡れ易さ(界面張力のバランス)という物質の性質によって決まる

Fluid geometry calculation

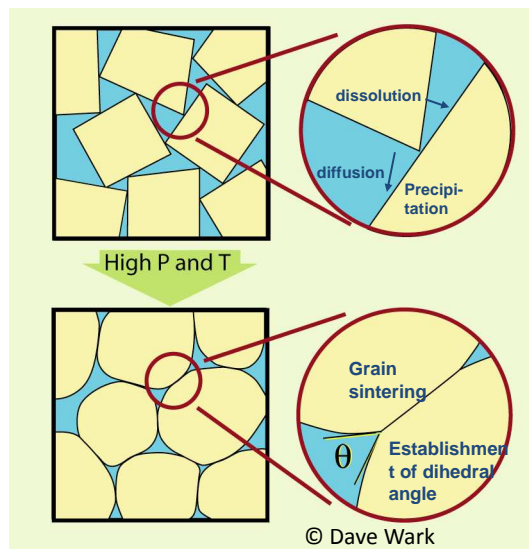


Equilibrium Microstructure ("textural equilibrium")

“組織平衡”
 溶解-沈殿作用による
 界面エネルギーの
 局所的な極小化

↑ 範囲は曖昧

必要な物質輸送の距離:
 個々のporeの組織平衡
 ~ poreサイズ
 << 実験産物全体の組織平衡
 ~ 実験産物のサイズ



表面(界面)張力

二つの相の境界面の面積を変えるためには仕事が必要になる。
 → 表面張力に対する仕事
 これを含めると、準静的過程に対するエネルギー変化は

$$dU = TdS - p'dV' - p''dV'' + \gamma d\sigma + \mu'dN' + \mu''dN''$$

p', p'' : 相1, 2内部の圧力
 $\mu'(T, p'), \mu''(T, p'')$: 各相の化学ポテンシャル
 σ : 境界面の面積
 N', N'' : 相1, 2内部の分子数

$$\gamma \equiv \left(\frac{\partial U}{\partial \sigma} \right)_{S, V', V'', N', N''}$$

表面張力に起因する圧力差

相1が半径 r の球であるとき

$$p' - p'' = \frac{2\gamma}{r} \quad \text{Laplaceの式}$$

$dS = dN' = dN'' = 0$ (断熱, 物質の生成消滅なし)
 $dV'' = -dV'$, $dV'/d\sigma = r/2$ という変形を考え,
 平衡条件 $dU = 0$ から導かれる。

例) 半径 r の液滴と蒸気圧 p_r との関係は

$$\mu_l(T, p_r + \frac{2\gamma}{r}) = \mu_g(T, p_r)$$

**Over what P-T conditions
can geometric adjustment occur?**

1. > Lowest metamorphic grade
(200-300 °C)
← Existence of fluid inclusions
(Fracture healing,
Grain boundary migration)
2. Healing Rate of Fracture & Cracks
> Plastic Deformation Rate
(Watson & Brenan, 1987, EPSL)
3. Fluid production rate < Dispersion rate
Segregation rate

Scaling Problems

e.g. Partially Molten Peridotite

Time Scale:

Equilibrium pore geometry is maintained at all times

Basalt in dunite (e.g., McKenzie, 1984)

$a = 10\mu\text{m} < 200\text{Hr}$ (Vaughan & Kohlstedt, 1982)

$a = 1\text{mm} < 10^3 \text{ yrs} \ll \text{Compaction time scale}$

Length Scale:

Basalt Infiltration into Dunite (1290°C) : 0.04-0.08 mm/hr

$W = 100\text{m}$ basalt sill may disperse in 200 yr (Watson 1982 Geology)

Cf. Aq. fluid into quartzite (823°C): 0.072 ± 0.018 mm/hr

(Nakamura & Watson 2001 Geofluids)

Carbonatite melt infiltration into dunite: $D = 1.8 \times 10^{-9} \text{ m}^2/\text{s}$

hundreds thousands of meters / 0.1 - 1 m.y.

(Hammouda & Laporte 2000 Geology)

岩石に保存されているfossil pore fluid geometry 1

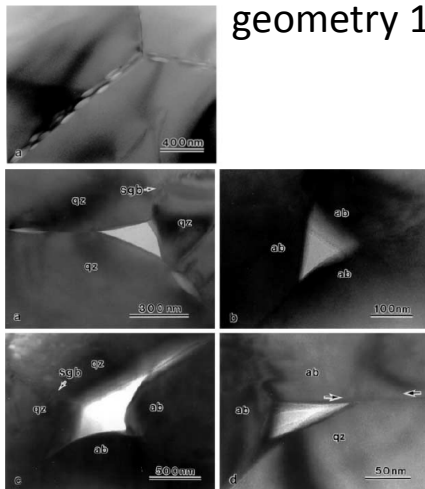


Fig. 2 TEM images of grain-edge pores in the calcite-free sample. a Pore at a junction of quartz grains with a sub-grain boundary (qb). b Pore at a junction of albite grains. c Pore at the junction of quartz and albite grains. d Pore at a junction of quartz and albite grains. At the region indicated by arrows, the plane of a quartz/albite boundary and pore/albite surface are on a straight line. e Pore at a junction of quartz grains with a sub-grain boundary formed by periodic array of dislocations

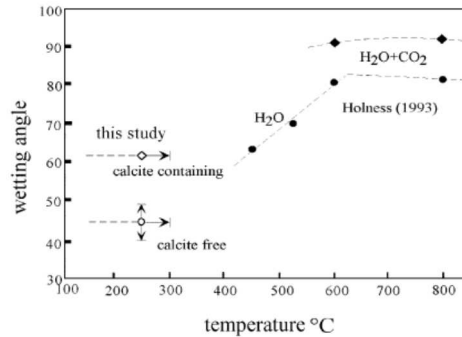


Fig. 8 Plot of wetting angle (quartz-fluid) variation with temperature at 400 MPa from Holness (1993) and comparing angles obtained in this study. The angles measured in this study are plotted at estimated ranges of temperature. Solid lateral lines correspond to ranges of peak metamorphic condition and dotted lines indicate the possible condition of formation of the wetting angles in the samples. Since there is some deviation between the peak and the median of our wetting angles, a range of values is indicated

Hiraga et al.
Contrib Mineral Petrol (2001) 141: 613–622

岩石に保存されているfossil pore fluid geometry 2

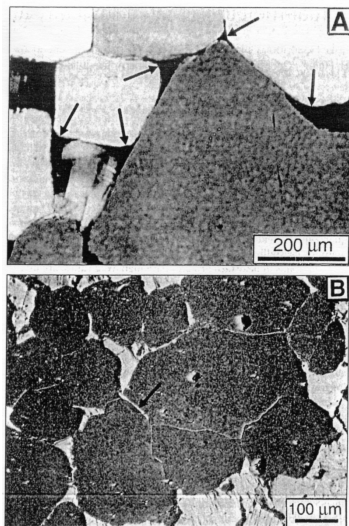


Figure 3. A: Micrograph of sample 9403 (location in Fig. 1) showing quartz grains with interstitial feldspar. Black arrows point to interstitial feldspar at quartz triple-grain junctions. B: Backscattered electron image of sample 9403 showing interstitial feldspar (light gray) at quartz (dark gray) triple junctions. Note curved phase boundaries between quartz and feldspar. Black arrow points to grain boundary entirely coated by feldspar.

Rosenberg & Riller (2000) Geology, 28, 7-10

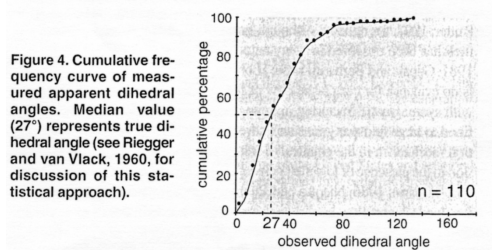
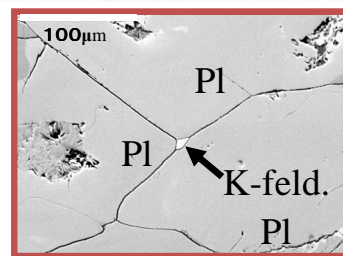


Figure 4. Cumulative frequency curve of measured apparent dihedral angles. Median value (27°) represents true dihedral angle (see Riegger and van Vlack, 1960, for discussion of this statistical approach).



阿武隈花崗岩 宮本複合岩体
(長谷部 2002 東北大修論)

急冷実験産物のpore fluid形状

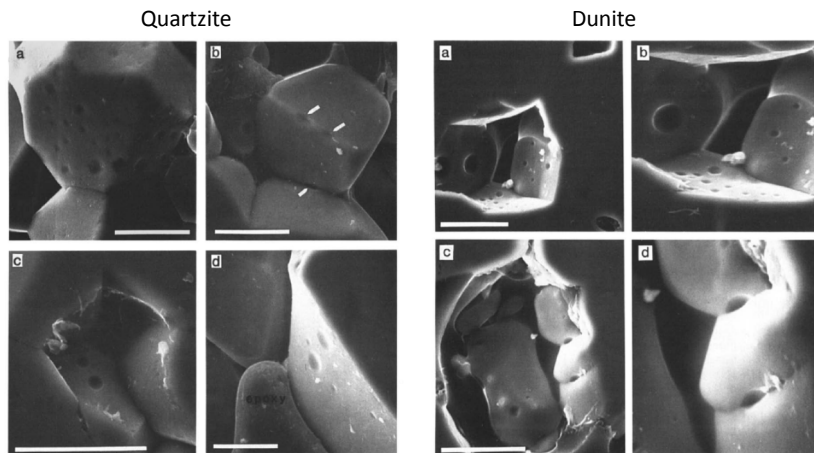


Fig. 5. Selected secondary-electron photomicrographs of regions in synthetic quartzites where grains have been plucked to reveal porosity features in three dimensions. Photo (a) is of run 3 (pure H_2O , $\theta = 57^\circ$); note the numerous surface dimples representing "casts" of once fluid-filled lozenges at grain boundaries. Note also the rounded nature of the grain edges, which formed the walls of fluid channels at run conditions (cf. Fig. 1). Photo (b) is of run 2 ($X_{CO_2} \sim 0.5$, $\theta = 70^\circ$); note the grain-edge "footballs" indicated by the arrows, and compare with the right-hand drawing in Fig. 1c. Photo (c), also of run 2, shows well-defined, apparently deeper dimples than those represented in (a), reflecting the higher wetting angle. The contrast in dimple form is most apparent in a comparison of (c) with (d), which was taken on quartz grains in run 15, in which $\theta \sim 40^\circ$. Note that all photos include some of the epoxy used to impregnate the samples. The white scale bars are 10 μm long. Watson & Brenan, 1987, EPSL

主な二面角(地殻～最上部マントル)

- ・メルト: ほぼ 60° 以下
- ・水: 60° 近傍～ 60° 以上(但し塩濃度の影響大)

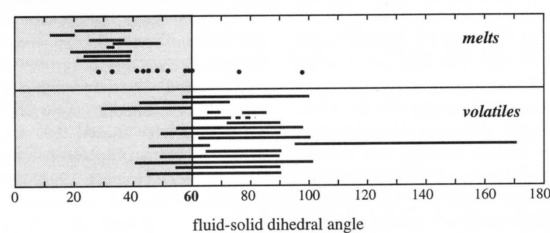


Figure 9.7 Experimentally determined fluid–solid dihedral angles in geological systems. Data are taken from Tables 9.2 and 9.3. Dots represent single reported values, lines show the ranges observed in systems as a function of pressure, temperature and fluid compositional variation. All melt data are $\leq 60^\circ$ apart from 2 isolated pyroxene values (Toramaru and Fujii, 1986) which were later shown to be too high (Fujii, Osamura and Takahashi, 1986; von Bargen and Waff, 1988). All volatile angles occupy a tight group between about 40° and 100° apart from one study (Hay and Evans, 1988) with angles ranging from 97° to 171° . They probably used an inappropriate measuring technique on poorly equilibrated samples (Holness and Graham, 1995). The only study with volatile angles almost exclusively $< 60^\circ$ was Lee, Mackwell and Brantley (1991) and their experiments were probably not fully texturally equilibrated (Brantley, 1992).

Holness (1997) *In*: Jamtveit B. & Yardley, B., Fluid flow and transport in rocks: Mechanisms and Effects, Chapman & Hall, 1977

Effect of fluid chemistry

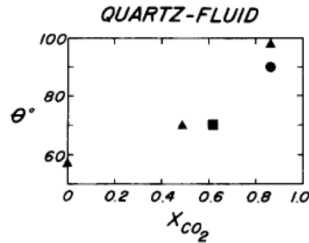


Fig. 3. Wetting angle (θ) vs. CO_2 mole fraction for "CO₂-H₂O" fluids in equilibrium with quartz. Strictly speaking, the fluids are not binary mixtures, but contain some CO at the oxygen fugacity intrinsic to our piston-cylinder assemblies (just below FMQ). The X_{CO_2} values are based on the calculations of Holloway and Reese [21]. Triangles: 950 °; squares: 1000 °; circles: 1150 ° C. See text and Fig. 2.

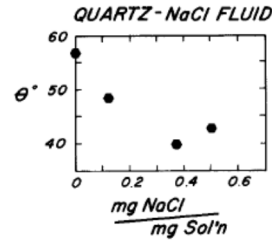


Fig. 12. Wetting angle (θ) vs. NaCl concentration in aqueous fluids in equilibrium with quartz at 1000 °C and 1 GPa.

Earth and Planetary Science Letters, 85 (1987) 497–515

Fluids in the lithosphere, 1. Experimentally-determined wetting characteristics of CO₂-H₂O fluids and their implications for fluid transport, host-rock physical properties, and fluid inclusion formation

E. Bruce Watson and James M. Brenan

Dihedral angles in the upper mantle 1

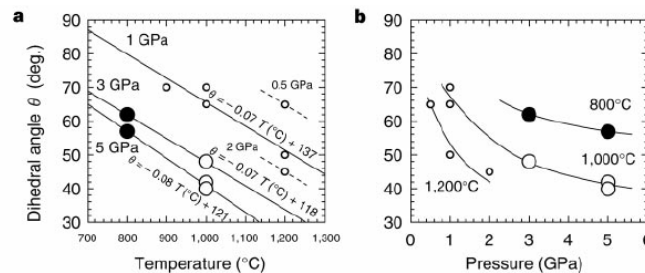
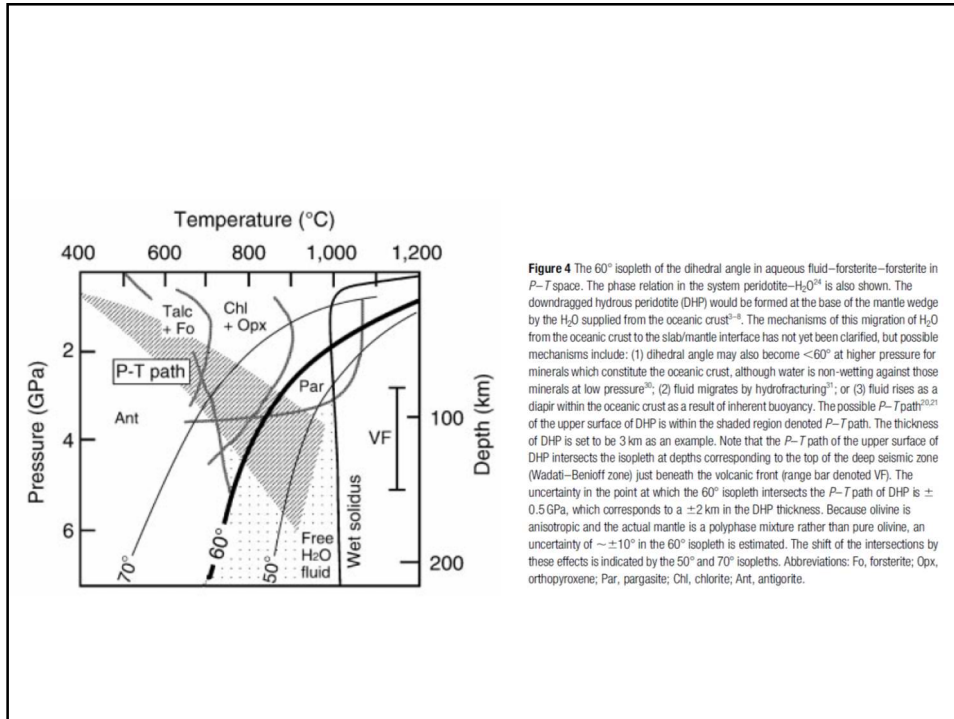


Figure 3 The aqueous fluid–forsterite–forsterite dihedral angle as a function of temperature and pressure. **a**, Temperature; **b**, pressure. The solid lines in **b** do not represent a fit to the data but are merely intended as a guide to the eye. The 800 °C and 1,200 °C curves in **b** are drawn to be consistent with the shape of the 1,000 °C curve. Large solid circle: this study. Large open circle: data from ref. 11. Small open circle: data from ref. 10.

Mibe et al., *Nature*, 1999



Dihedral angles in upper mantle 2

S. Ono et al. / Earth and Planetary Science Letters 203 (2002) 895–903

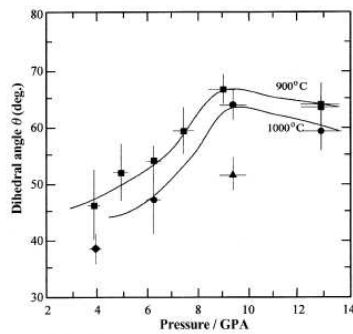


Fig. 3. Dihedral angle versus pressure diagram. The plotted value of the dihedral angle is the median angle. Squares, 900°C; circles, 1000°C; triangle, 1100°C; diamond, 1200°C. The contours are schematic.

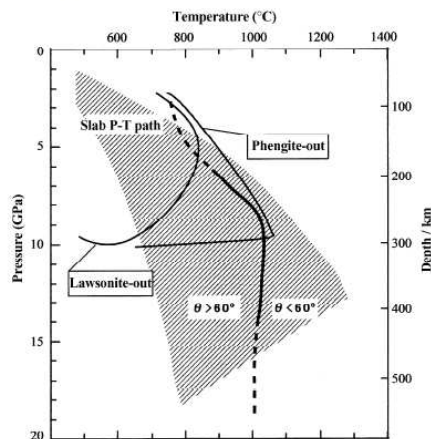


Fig. 4. 60° isopleth of the dihedral angle in fluid–pyrope–pyrope in P – T space. The limit of lawsonite and phengite breakdown in the system MORB– H_2O [11,15] is also shown. The possible P – T path of the upper part of the subducted oceanic crust is shown as the shaded region.

Requirements to Minimize Total Interfacial Energy

- Dihedral angle
- Equilibrium fluid fraction
- Uniform mean curvature
- Minimum interfacial area



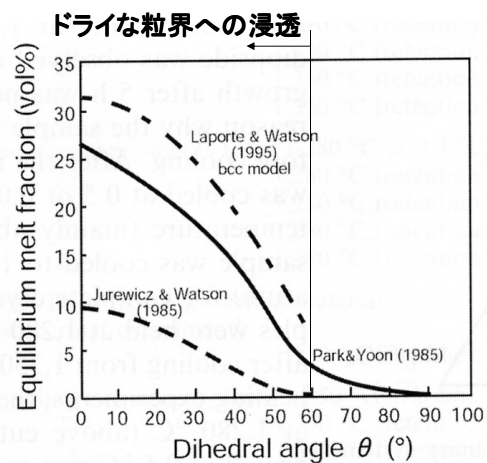
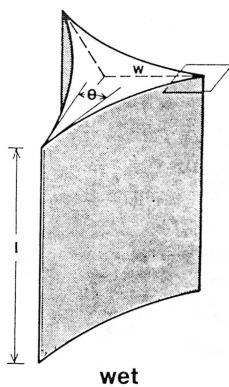
Texture Rearrangements

- GB grooving
- Fluid infiltration / Expulsion
- Grain size effect
- Grain growth / Ostwald ripening

Minimum Energy Fluid Fraction

(MEMF, equilibrium melt fraction)

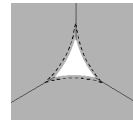
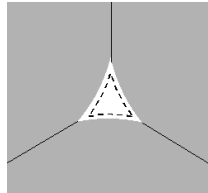
二面角が小さい＝固液界面エネルギーが小さい
＝結晶粒界に流体が浸透すると系のエネルギーが下がる



“Grain Size Effect” on the Equilibrium Porosity

Large Curvature

Small Curvature

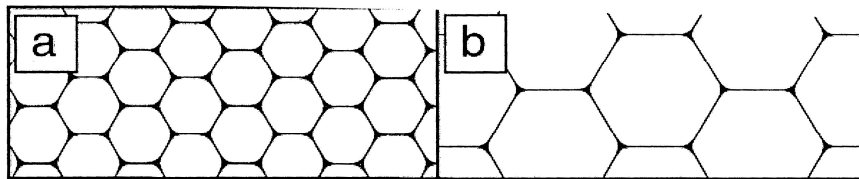


Precipitation $\xleftarrow{\text{flux}}$ Solution

$$\mu_{coarse} < \mu_{fine}$$

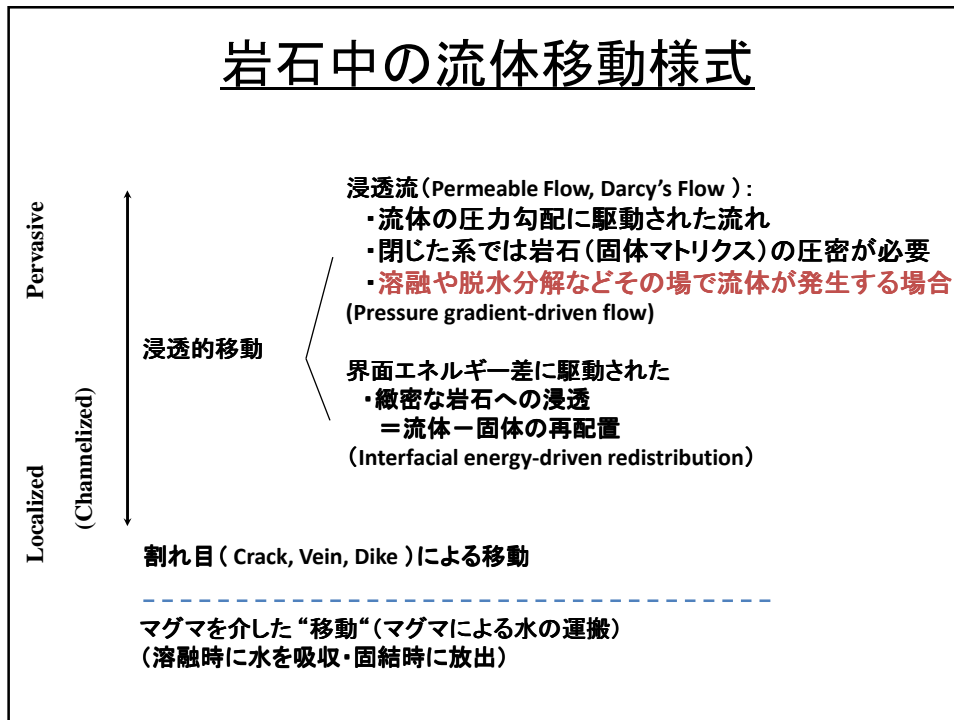
Wark & Watson, 1999

流体量分布の粒径による効果



- θ (二面角)、 κ (界面曲率) が同じならば必然的に粒子の大きさに因らず pore の大きさは同じになる。
→ 細粒領域の方が pore の数が多くなるので、流体量も細粒領域のほうが多くなる。

岩石中の流体移動様式



固液共存系における物質輸送の素過程

流体力学的流れ (flow)

- >> 流体ネットワーク中の拡散
- >> 粒界拡散 (grain boundary diffusion)
- >> 鉱物内の拡散 (lattice diffusion)

ダルシーの法則

流束 \propto 流体の圧力勾配

$$Q = \frac{k}{\eta} \frac{\Delta p}{d}$$

k : 浸透係数 Permeability

η : 流体の粘度

Large scale fluid migration

...should be rate-limited by
 permeability, fluid viscosity, pressure gradient
 deformation rate of solid matrix
 (interfacial energy-driven fluid redistribution is not effective for km-scale fluid migration)

If so,
What is the principal effect of surface energy?
 = Controlling melt interconnectivity and permeability

Indirect, but major influence on the large scale fluid motions (e.g., Waff, 1980, McKezie, 1984, Stevenson, 1986)

Theory (Geometric Adjustment)

- **Pressure difference across a curved surface**

(Kingery et al., 1975)

$$\Delta P = \gamma \left(\frac{1}{r_1} + \frac{1}{r_2} \right) \quad r_1, r_2 : \text{principal radii of curvature}$$

- **Solubility increase due to an applied pressure**

(Thomson-Freundlich equation)

$$\ln \frac{X\kappa}{X_0\kappa_0} = \frac{M\gamma}{\rho RT} \frac{1}{r}$$

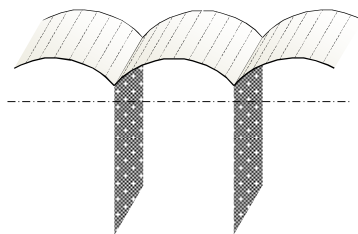
Solubility, Activity coeff.
over

X, κ : curved surface
 X_0, κ_0 : flat surface

M : molecular weight
 γ : interfacial energy
 ρ : density
 r : radii of curvature

Theory (Grooving Kinetics)

2-D Grain Boundary



$$d = 1.13 \frac{1}{\tan \Theta/2} (At)^{\frac{1}{2}}$$

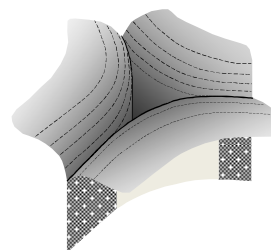
Dissolution-Precipitation
Control

$$d = 0.937 \frac{1}{\tan \Theta/2} (Bt)^{\frac{1}{4}}$$

Surface Diffusion
Control

(Mullins, 1957)

Triple Junction



Geofluids (2001) 1, 73–89

Experimental study of aqueous fluid infiltration into quartzite: implications for the kinetics of fluid redistribution and grain growth driven by interfacial energy reduction

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